# **Crystallization of running filament in melt spinning of polypropylene**

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The crystallization kinetics of the running filament in melt spinning have been studied for three cases: isothermal crystallization of an isotropic melt, non-isothermal crystallization of an isotropic melt, and non-isothermal crystallization of a non-isotropic melt, Both the temperature and the orientation dependences of nucleation rate and growth rate are estimated for polypropylene. Calculated curves for non-isothermal crystallization of a non-isotropic melt with partial high orientation closely approximate the experimental data. In particular, the experimental data are best explained by crystallization with two-dimensional growth. The crystallization processes in melt spinning may be governed by localized molecular orientation of the supercooled melt in the initial stage.

### **INTRODUCTION**

Generally, solidification during the melt spinning of crystallizable polymer is non-isothermal crystallization of a nonisotropic melt. Little work has been reported on the kinetics of crystallization of the running filament in melt spinning because here crystallization is very much faster than isothermal crystallization of the isotropic state. However, many papers have reported on the isothermal crystallization of isotropic melts. Non-isothermal crystallization of an isotropic melt has been studied by several investigators. Comparison of theory and experiment has been reported on the Here  $X_{\infty}$  is crystallinity at the termination of the crystalliza-<br>variation of crystallinity of as-spun filaments<sup>1,2</sup>, on the cry-<br>tion process,  $\rho_c$  and  $\rho$ stallization of poly(ethylene terephthalate) using differential liquid phase, respectively,  $G(u)$  is the rate of linear growth thermal analysis<sup>3</sup>, and on the crystallization of polyethylene at time u,  $N(\tau)$  is the rate using X-ray diffraction<sup>4-6</sup>. On the other hand, in isothermal is the shape factor and n is a constant. crystallization of a non-isotropic melt, the molecular orien-<br>tational effect on rate of crystallization is significant. The melt, one assumes that G and  $\dot{N}$  are constants. This assum increase in crystallization rate can be divided into two parts, tion reduces equation (1) to: nucleation rate and growth rate; it has been theoretically estimated for molten polyethylene subjected to a constant shear stress<sup>7</sup>.

In this work, the changes of crystallinity and of noncrystalline orientation along the spinning direction were crystallization of an isotropic melt, non-isothermal crystal-<br>lization of an isotropic melt, and non-isothermal crystalliza-<br>he pop-isothermal crystallization from a non-isothermal crystallization from a non-isothermal cry lization of an isotropic melt, and non-isothermal crystallization from a non-isotropic<br>tion of a non-isotropic melt. Data on nucleation rate and<br> $m$ <sup>1</sup> C and  $\dot{N}$  are dependent on the aristallization terms growth rate are required for the study of the kinetics as ture  $(T)$  and the molecular orientation of non-crystalline functions of crystallization temperature and nonfunctions of crystallization temperature and non-<br>crystalline orientation. The temperature dependence of exploring presence  $\sum_{n=1}^{\infty}$  which are functions of time in the meltcrystalline orientation. The temperature dependence of spinning process. That is to say, the rate of nucleus forma-<br>nucleation rate and growth rate for polypropylene (PP) was tion at time a from the enimerate in  $N(T<sub>C</sub>)$ 

theory the degree of transformation at time t amounts to: with equation  $(1)$ . For a homogeneously nucleated system:

$$
- \ln \left( 1 - \frac{X}{X_{\infty}} \right) = \frac{1}{X_{\infty}} \frac{\rho_c}{\rho_l} \int_{0}^{t} v(t, \tau) \dot{N}(\tau) d\tau
$$
  

$$
v(t, \tau) = k_f \left[ \int_{-\tau}^{t} G(u) du \right]^{n}
$$
 (1)

tion process,  $\rho_c$  and  $\rho_l$  are the density of the crystalline and at time u,  $N(\tau)$  is the rate of nucleus formation at time  $\tau$ ,  $k_f$ 

melt, one assumes that G and  $\dot{N}$  are constants. This assump-

$$
-1\mathbf{n}\left(1-\frac{X}{X_{\infty}}\right)=\frac{1}{X_{\infty}}\frac{\rho_c}{\rho_i}Kt^n\tag{2}
$$

In this case, the crystallization kinetics can be analysed by

tion of a non-isotropic metr. Data on nucleation rate and melt, G and N are dependent on the crystallization tempera-<br>growth rate are required for the study of the kinetics as  $\frac{m}{\sqrt{n}}$  and the malendar arisettion of a tion at time  $\tau$  from the spinneret is  $N[T(\tau), \Delta n_a(\tau)]$ , and the derived from many data on isothermal crystallization  $2^{2}-27$ .<br>The orientation dependence of these was also calculated.<br> $\Delta x$  (i)]. Then we get a growth at time u from the spinneret is  $G[T(u)]$ ,  $\Delta n_a(u)$ . Then we may consider that the nucleus which was originated at time  $\tau$  is growing up to observed time  $t$ THEORY THEORY (=  $p\Delta t$ ) with the various linear growth rate of  $G_i[T(u)]$ ,  $\Delta n_a(u)$ . Here p is the number of time intervals  $\Delta t$ . In this We start from the theory of phase transformations proposed case the degree of crystallini, y X at time t along the spinning by Avrami<sup>8,9</sup> and Mandelkern *et al.*<sup>10</sup>. According to this path can be obtained as the followi path can be obtained as the following expressions by analogy

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$$
-1n\left(1-\frac{X}{X_{\infty}}\right) = \frac{1}{X_{\infty}}\frac{\rho_c}{\rho_l}k_f\sum_{i=0}^{P}x
$$

$$
\left(\sum_{j=i}^{P}G_j[T(u),\Delta n_a(u)]\Delta t\right)^n\dot{N}_i[T(\tau),\Delta n_a(\tau)]\Delta t \qquad (3)
$$

For a heterogeneously nucleated system: RESULTS AND DISCUSSION

$$
- \ln\left(1 - \frac{X}{X_{\infty}}\right) = \frac{1}{X_{\infty}} \frac{\rho_c}{\rho_l} k_f \sum_{i=0}^{p} \times \left\{\sum_{j=i}^{p} G_j[T(u), \Delta n_a(u)] \Delta t \right\}^n \overline{N}_i[T(\tau), \Delta n_a(\tau)] \tag{4}
$$

Additionally, in non-isothermal crystallization from an small, in the order of  $0.5-1$  sec. At the onset of crystalliza-<br>isotropic melt, G and N are dependent on crystallization<br>isotropic melt, G and N are dependent on cr isotropic melt, G and N are dependent on crystallization tion, attenuation of the running filament is still in process<br>temperature and independent of orientation. Therefore, temperature and independent of orientation. Therefore, and the first half of crystallization proceeds under longitu-<br> $X(t)$  is calculated assuming that  $\Delta n_a(t)$  at time t may be zero dinel deformation. The crystalline orie  $X(t)$  is calculated assuming that  $\Delta n_a(t)$  at time t may be zero dinal deformation. The crystalline orientation factor and in equation (3) or (4).

The sample used in this study was commercial polypropylene orientation of the non-crystalline component indicates a<br>of intrinsic viscosity  $[\eta] = 2.2$  dl/g determined in decalin at minimum and negative value such as the re of intrinsic viscosity  $[\eta] = 2.2$  dl/g determined in decalin at minimum and negative value such as the results at low elongation of drawing<sup>15,16</sup>. This may be interpreted in 135°C. The polymer melt was extruded at 250°C by a elongation of drawing <sup>15,16</sup>. This may be interpreted in regulated constant nitrogen pressure through a die fitted therms of loosening of the chain in the non-crystallin regulated constant nitrogen pressure through a die fitted terms of loosening of the chain in the non-crystalline part<br>with a single orifice. The die diameter was 2 mm, extrusion by heat of crystallization<sup>14</sup>. In the final with a single orifice. The die diameter was 2 mm, extrusion by heat of crystallization<sup>14</sup>. In the final stage of crystalliza-<br>rate 0.4 g/sec and stretch ratio 59 or 240. The extruded tion, the molecular orientation of th rate 0.4 g/sec and stretch ratio 59 or 240. The extruded tion, the molecular orientation of the non-crystalline com-<br>fibre was passed through a diffractometer with a rotating-<br>nonent decreases with the progress of crystall fibre was passed through a diffractometer with a rotating-<br>anode X-ray generator and was wound onto a take-up device<br>can be accounted for by the concentration of strain from anode X-ray generator and was wound onto a take-up device can be accounted for by the concentration of strain from with speed of 10 m/min or 40 m/min. Wide-angle X-ray dif-<br> $\frac{1}{2}$  recorreceive crystallites around the n fraction patterns were obtained along the spinning path to a distance of 100 cm from the spinneret. In this measurement, the X-ray was conducted on the moving filament during processing.  $CuK\alpha$  radiation through a Ni filter was used. 60 The working conditions were 40 kV, 100 mA. The separation of amorphous scattering from the crystalline peaks was made by the method suggested by Natta *et aL 11.* Data on the crystal orientation and the degree of crystallinity were obtained from (110), (040) and (111) reflections. The X-ray diffraction curve at a distance of 100 cm from the spinneret 40 was almost the same as that of the take-up filament. The degree of crystallinity of the take-up filament, derived from<br>density measurement, was 60%. The running filament was density measurement, was 60%. The running filament was photographed through the microscope at magnifications of  $100\times$  and the diameter d determined.

The temperature distribution was evaluated using  $20$ Ziabicki's procedure<sup>12</sup>. The time from the spinneret was calculated from the diameter profile

$$
t = \int_{0}^{x} 1/V \mathrm{d}x = \pi/4Q \int_{0}^{x} d^2 \mathrm{d}x
$$

The birefringence of the running filament was measured as *Figure 1* Variation of crystallinity X along the spinning path for a function of position along the spinning path. The bire-<br>take-up velocities of 40 m/min (O) and 10 m/min ( $\bullet$ )

fringence was determined by measurement in a polarization microscope using a Bereck compensator. Both the crystalline and non-crystalline components of a polymer contributed to the measured birefringence. The molecular orientation of the non-crystalline component  $(\Delta n_a)$  was estimated from a combination of the X-ray diffraction measurement with the birefringence. More detailed descriptions of the equipment and procedure have been given elsewhere<sup>13,14</sup>.

#### *p Crystallization behaviour ofrunningfilament*

The X-ray diffraction curves at 20 cm from the spinneret show a liquid or amorphous halo. At 25 cm from the spinnet, crystalline peaks are recognized in the X-ray diffraction curve. The variation of crystallinity along the spinning {~ ) n path obtained by X-ray diffraction is shown in *Figure 1.*  The crystallization begins at a point 22-25 cm from the spinneret, and the degrees of crystallinity at 60-100 cm are similar to that of the take-up fibre. The residence time in the region of rapid development of crystallization is very the fraction of  $a^*$ -axis-oriented crystallite are not changed throughout the crystallization process $<sup>13</sup>$ .</sup>

The distributions of temperature and molecular orienta-EXPERIMENTAL tion of the non-crystalline component  $(\Delta n_a)$  are shown in *Figure 2.* In the initial stage of crystallization, molecular progressive crystallites around the non-crystalline chain<sup>14</sup>.





 $\Delta n_a$  of running filament with time from spinneret

## *Isothermal crystallization of isotropic melt a*

the most simplified case of crystallization in running filaments during melt spinning. Two different results have been published for the temperature distribution along the  $\circ$ spinning path. One of these is that the heat of crystallization can be neglected<sup>11,17</sup>; the other is that it cannot<sup>18,19</sup>. In the latter, the temperature of the filament is kept constant in the early stages of crystallization because of the balance between heat released by crystallization and that lost by cooling. In the first, we will deal with the early stages of crystallization during melt spinni balance between heat released by crystallization and that  $\frac{3}{2}$   $\frac{2}{2}$ lost by cooling. In the first, we will deal with the early  $\frac{1}{2}$   $\left| \frac{\mathbf{b}}{\mathbf{b}} \right|$  -3  $\frac{-2}{2}$  -i stages of crystallization during melt spinning as an isother- mal crystallization.

*Figure 3* shows the Avrami plots of  $ln[-ln(1 - X/X_{\infty})]$ against 1n t for take-up velocities  $(V_E)$  of 10 m/min and 40 m/min, respectively. Time  $t$  of crystallization in the Avrami plots is usually regarded as the time interval from the instant  $(t = 0)$  when crystallization temperature is attained. For the running filament of melt spinning, however, the O determination of that time is very difficult. Four cases in *Figure 3* are chosen as follows: one,  $t = 0$  at the time when the filament is cooled to the melting point; the second,  $t = 0$ at the time when the crystallization is apparently observed. The others are arbitrarily chosen between these two points.<br>In Figure 3, the data points fall upon a straight line for an  $-2$  -  $-1$  0 In *Figure 3*, the data points fall upon a straight line for an early stage of crystallization. The results for Avrami's expo- in the secharal stage of crystallization. The results for Avrami's exponent *n* as functions of the start points in crystallization are *Figure 3* Plot of  $1n(-1n(1 - X/X_{\infty}))$  against  $1nr$ . (a) Take-up summarized in *Table 1* in which the start points are given velocity  $10 m/min$ ;  $\nabla$ ,  $t_0 = 9.4$ summarized in *Table l* in which the start points are given velocity 10 m/min;  $\nabla$ ,  $t_0 = 9.441$  sec,  $T_0 = 155^{\circ}$ C;  $\triangle$ ,  $t_0 = 9.370$  by the time  $(t_0)$  from the spinneret and by the temperature sec,  $T_0 = 159^{\circ}$ C by the time  $(t_0)$  from the spinneret and by the temperature  $(T<sub>0</sub>)$  of the running filament at this point. Supposing that the start point of crystallization lies in the time when the crystallization is apparently observed, the slopes and the intercepts of these lines give values of  $n = 1.1$  and  $K = 1.1$  sec<sup>-1</sup>  $(V_E = 10 \text{ m/min})$  or  $K = 2.9 \text{ sec}^{-1}(V_E = 40 \text{ m/min})$ . *Table 1* Set of *n* for the start point of crystallization The exponent  $n = 1$  is in agreement with results reported by other investigators for the rate of oriented crystallization of natural rubber<sup>20</sup> and crosslinked polyethylene<sup>21</sup>. This would imply heterogenous nucleation with concurrent onedimensional linear growth<sup>9</sup>. The values of the crystallization rate constants of a running filament are much higher than those of general crystallization. Moreover the crystallization rate constant at high take-up velocity is larger than that at

low take-up velocity. The results show that molecular orientation by extension accelerates crystallization. However, on the assumption that the start point of crystallization is in the  $200<sup>1</sup>$  time when the filament is cooled to the melting point, the value of  $n = 3$  is obtained, which is very similar to the results of isothermal crystallization from an isotropic melt for polypropylene $^{22-25}$ .

Data for crystallization rate constant  $K$  and linear growth  $100$   $\bigcup_{\text{rate constant } G \text{ have been reported by several investigations}$ for polypropylene<sup>22-27</sup>. However, the temperature dependence of  $K$  and  $G$  for polypropylene have not been expressed as a general formula over a wide temperature range. On the other hand, for poly(ethylene succinate), natural rubber and nylon-6, this has been expressed by Takayanagi and Kusu-  $\frac{1}{7}$  ,  $\frac{1}{8}$  ,  $\frac{1}{8}$  ,  $\frac{1}{100}$  ,  $\frac{1}{100}$  and  $\frac{1}{100}$  and  $\frac{1}{100}$  and  $\frac{1}{100}$  and  $\frac{1}{100}$  from existing data for commercial  $\begin{array}{ccc}\n6 & 7 \\
\hline\n6 & 1000 & 1100 \\
\end{array}$  ture dependence of K and G from existing data for commercial Figure 2 Variation of temperature T and orientation parameter polypropylene. It was assumed by them that the  $(T_m/T)(1/\Delta T)$ <br>Law is applicable to the term of the critical nucleus forma*law* is applicable to the term of the critical nucleus forma-



T<sub>O</sub> = 184°C. (b) Take-up velocity 40 m/min;  $\nabla$ ,  $t_0 = 7.223$  sec,<br>  $T_0 = 132^{\circ}$ C;  $\bullet$ ,  $t_0 = 7.168$  sec,  $T_0 = 145^{\circ}$ C;  $\bullet$ ,  $t_0 = 7.147$  sec,  $T_0$ <br>
= 150°C;  $\bullet$ ,  $t_0 = 6.930$  sec,  $T_0 = 180^{\circ}$ C

$V = 10$ m/min			$V = 40 \, \text{m/min}$		
$t_0$ (sec)	$T_0$ (°C)	n	$t_0$ (sec)	$T_0(^{\circ}C)$	n
9.441	155	1.1	7.223	132	1.1
9.370	159	1.3	7.168	145	1.4
9.276	163	1.5	7.147	150	1.5
8.863	184	3.3	6.930	180	3.1



*Figure 4* Plot of log *K* + 337.57/( $T - 221.4$ )<sup>2</sup> *versus*  $T_m/T_A$  for On the other hand, the melting point  $(T_{m0})$  in an orientcommercial PP:  $\bullet$ , Ishizuka <sup>22</sup>, O, Magil<sup>23</sup>;  $\blacktriangle$ , Iwanami *et al.*<sup>24</sup>;  $\triangle$ , ed polymer system can be written as: Marker *et al. 2s* 

tion and the activation energies for transport across the liquid-crystal interface are proportional to the activation energy of flow obtained from WLF equation. Then the temperature dependences of  $K$ ,  $G$  and  $N$  can be expressed as:

$$
\ln K = \ln K_c - \frac{m\rho C_1 T}{(T - C_2)^2} - \frac{(mC_3 + C_4)T_m}{T\Delta T}
$$
  

$$
\ln G = \ln G_c - \frac{\rho C_1 T}{(T - C_2)^2} - \frac{C_3 T_m}{T\Delta T}
$$
 (5)

$$
1n\dot{N}=1n\dot{N}_c-\frac{\rho C_1 T}{(T-C_2)^2}-\frac{C_3 T_m}{T\Delta T}
$$

where  $\rho$ ,  $C_1$  and  $C_2$  are constant, m is an integer that de-<br>pends upon the geometry of the growth process, and  $C_3$ <br>and  $C_4$  are estimated from plots of  $\ln K + mC_1T/(T - C_2)^2$ <br>against  $T_m/T\Delta T$  and  $\ln G + C_1T/(T - C_2)^2$ pends upon the geometry of the growth process, and  $C_3$ and  $C_4$  are estimated from plots of  $\ln K + mC_1T/(T - C_2)^2$ against  $T_m/T\Delta T$  and  $\ln G + C_1T/(T - C_2)^2$  against  $T_m/T\Delta T$ . The former plots, from data for commercial polypropylene obtained by several investigators, are illustrated in *Figure 4. ? ~* 

by different methods of many investigators, a straight line may be drawn through the data points. The plots of  $\ln G + C_1 T/(T - C_2)^2$  against  $T_m/T\Delta T$  can be also obtained as a straight line. For the isothermal crystallization of polypropylene, Avrami's exponent  $n = 3$  has been reported by  $\begin{array}{c} \n\sqrt{3} & \text{if } \frac{1}{2} & \text{if }$ several investigators<sup>22–2s</sup> and it would imply a heterogeneous  $\sim$  40 80 120 160 160 nucleation with concurrent three-dimensional growth. In  $\tau$  (°C) this case  $\dot{N}$  in equation (5) can be replaced by the number<br>of heterogeneous nuclei  $\bar{N}$  which may be similarly dependent on temperature. Both these results and data are illustrated in *Figure 5.* Figure 4

### *Orientation dependence of crystallization rate constnat*

Polymer molecules are considered to be deformed by deformation of the polymer melt, and their entropy is usually  $5<sup>h</sup>$  decreased. The decrease in entropy of the melt allows crystallization to occur at a higher temperature than would nor mally be observed for the same substance in the absence of any deformation. The effects of G and  $\dot{N}$  in such a condition have been evaluated for isothermal crystallization under shear deformation of polyethylene by Kobayashi and axial deformation of polypropylene.

> Assuming a Gaussian chain, the orientation and the decrease in entropy for the polymer melt with extension ratio  $(\lambda)$  are given by:

$$
\Delta n_a = \frac{2\pi}{45} \frac{(n^2 + 2)^2}{n} N(\alpha_1 - \alpha_2) (\lambda^2 - \frac{1}{\lambda})
$$
 (6)

$$
\Delta s_o = -\frac{NK}{2}(\lambda^2 + \frac{2}{\lambda} - 3) \tag{7}
$$

 $\frac{1}{2}$  a  $\frac{1}{3}$  number of polymer segments per unit volume, and  $\alpha_1 - \alpha_2$ <br>is the difference of principal refractive indices. For poly-2 3 is the difference of principal refractive indices. For poly-<br>  $T_m/T\Delta T \times 10^{2}$  (K<sup>-1</sup>) propylene  $\alpha_1 - \alpha_2 = 3.602 \times 10^{-25}$ , and *n* and *N* are given propylene  $\alpha_1 - \alpha_2 = 3.602 \times 10^{-25}$ , and *n* and *N* are given as functions of density.

$$
T_{mo} = \frac{\Delta s}{\Delta s - \Delta s_o} T_m \tag{8}
$$



*Figure 5* Plots of *K* (A);  $G^3$  (B) and  $\overline{N}$  (C) *versus* crystallization temperature *T.* ----, calculated from equation (5). **E**, Marker *et*  $aL^{25}$ ;  $\Box$ , Padden *et al.*<sup>26</sup>; X, Hoshino *et al.*<sup>27</sup>; other sy



*Figure 6* Melting temperature in oriented system of polypropylene In non-isothermal crystallization of an oriented melt, the as a function of time as a function of non-crystal orientation parameter  $\Delta n_a$ . The line is growth rate and the number of nuclei as a function of time calculated from equations (6), (7) and (8)



*Figure 7* Variation of G  $\left( \frac{1}{\sqrt{N}} \right)$  and  $\overline{N}$   $\left( \frac{1}{\sqrt{N}} - \frac{1}{\sqrt{N}} \right)$  with crystallization temperature for various orientation parameters  $\Delta n_a$ : A, E,  $\Delta n_a$  $= 10 \times 10^{-3}$ ; B, F,  $\Delta n_a = 5.7 \times 10^{-3}$ ; C, G,  $\Delta n_a = 2.0 \times 10^{-3}$ ;  $\mathcal{L}$ ,  $\mathcal{L}$ ,  $\mathcal{L}$  if  $\mathcal{L}$ 

The variation of melting point  $(T_{mo})$  with non-crystalline the theory of the theory of (sec) orientation parameter  $(\Delta n_a)$  is shown in Figure 6 for  $\Delta s =$ <br>3.92 x 10<sup>6</sup>erg/cm<sup>3</sup> °C <sup>30</sup>. By substitution of *T<sub>mo</sub>* into perimental data ( $\bullet$ ), theoretical value (-----) in the non-isothermal<br>equation (5) both the te equation (5) both the temperature and orientation dependences of  $G(T, \Delta n_a)$  and  $\overline{N}(T, \Delta n_a)$  can be obtained. These dimensional growth; B,B', two-dimensional growth; C,C', oneresults are plotted against  $T$  for several different values of dimensional growth

 $\Delta n_a$  in *Figure 7.* If the horizontal axis in *Figure 7* is replaced by  $\Delta n_q$ , it is shown in the Figure that  $G(T, \Delta n_q)$  and

#### *Non-isothermal crystallization in melt spinning*

First, we deal with non-isothermal crystallization of an isotropic melt. The growth rate and the number of nuclei as a function of time from the spinneret can be estimated ture in *Figure 2.* Then, assuming that  $\Delta n_a(t)$  is zero in equation (4), the degree of crystallinity is calculated along the spinning path. A plot of the calculated values against time from spinneret is shown in *Figure 8* together with the results using the X-ray diffraction method. Here, in calculating these curves, the values of shape factor of equation 5OO (4) used are  $k_f = 4\pi/3$  for three-dimensional growth,  $k_f = \pi l_c$  $(l_c = 150 \text{ Å})$  for two-dimensional growth, or  $k_f =$  $1/2\pi d_c^2$  ( $d_c$  = 1000 Å) for one-dimensional growth. The  $\overline{a}$   $\overline{a}$   $\overline{a}$   $\overline{a}$   $\overline{a}$   $\overline{a}$  calculated curves cannot be reconciled with the experimen- $\Delta n_{\sigma}$  **x** IO<sup>3</sup> **ightarrow is talled to the set of the actual crystallization during**  $\Delta n_{\sigma}$  **<b>x** IO<sup>3</sup> melt spinning occurs extremely fast.

from spinneret can be estimated from combination of *Figure* 7 with *Figure 2.* The degree of crystallinity is then calculated by using equation (4). The results are shown in *Figure 8.*   $\overline{A}$  The parameters utilized in the calculation are the same as in the case of non-isothermal crystallization of an isotropic melt. The calculated curves are still not fitted by the experimental data. The effect of orientation is apparent, however,  $\overline{10^2}$  B by comparison of the results for non-isothermal crystallization in an isotropic melt.

> On the other hand, constant molecular orientation of the crystalline component  $(\Delta n_c)$  was obtained throughout the crystallization process<sup>13</sup>. The molecular orientation



Figure 8 Variation of crystallinity X along the spinning way for exnon-isothermal crystallization of non-isotropic melt; A,A', three-



Figure 9 Variation of crystallinity X along the spinning way for<br>experimental data ( $\bullet$ ) and theoretical value  $\begin{array}{c} 4 \\ - \end{array}$  in the non-<br>isothermal crystallization of non-isotropic melt with a constant<br>crystallizabl crystallizable molecular orientation: A, three-dimensional growth, *An<sub>a</sub>* = 0.004; B, two-dimensional growth, *Δn<sub>a</sub>* = 0.0065; C, one-<br>dimensional growth *Δn<sub>a</sub>* = 0.013<br>*J. Appl. Polym. Sci. 1974, 18,61926bi. <i>V. and Negesue* T. *I.* 

city of 40 m/min. From this result it may be inferred that 10 Mandelkern, L. 'Crystal<br>the orientation of 'crystallizable molecules' is constant New York, 1964, Ch. 8 the orientation of 'crystallizable molecules' is constant<br>throughtout the crystallization process. The degree of crys. [1] Natta, G., Corradini, P. and Cesari, M. Atti. Accad. Naz. throughtout the crystallization process. The degree of crystallinity is calculated assuming that  $\Delta n_a(t)$  is constant in  $12$ equation (4). The growth rate, and the number of nuclei in  $\frac{Vol(1, Ch.5)}{Vol(1, Ch.5)}$ the melt with constant orientation, are obtained from 13 Ishizuka, O. and Koyama, K. *Sen'i Gakkaishi* 1976, 32, T43<br>Figure 7 as functions of temperature. The growth rate 14 Ishizuka, O. and Koyama, K. *Sen'i Gakkaishi* 19 *Figure 7* as functions of temperature. The growth rate 14 Ishizuka, O. and Koyama, K. *Sen'i Gakkaishi* 1976, 32, T49  $(G[T(t), \Delta n_a(t)])$  and the number of nuclei  $(N[T(t), \Delta n_a(t)])$ .  $\Delta n_a(t)$ ] at a time t from the spinneret can be estimated for Samuels, R. J. J. *Polym. Sci.* 1965, 3, 1741 from a combination of the temperature dependence with  $\Delta n_a(s)$ . The Samuels, R. J. J. *Polym. Sci.* (A) 1965. 3, from a combination of the temperature dependence with 17 Kase, S. and Matsuo, T. J. Polym. Sci. (A) 1965. 3, 2541<br>the distribution of temperature along the spinning path in 18 Katayama, K., Amano, T. and Nakamura, T. Kollo the distribution of temperature along the spinning path in *Figure 2.* Substituting  $G[T(t), \Delta n_a(t)]$  and  $N[T(t), \Delta n_a(t)]$  <sup>220,125</sup> <sub>Spruiell, J. E. and White, J. L. Appl. Polym. Symp. 1975, 27,</sub> into equation (4), the degree of crystallinity can be calculat-  $\frac{121}{121}$ ed as a function of time from the spinneret. The results are 20 Kim, Hyo-gun and Mandelkern, L. J. Polym. Sci. 1967, 6, 181<br>shown in *Figure* 9 Here in calculating these curves, the 21 Kitamaru, R. and Chu, H. D. Bull. Ins shown in *Figure 9.* Here, in calculating these curves, the 21 Kitamaru, R. and Chu, H. Bull. lnst. Chem. Res. Ag. 97 following values of non-crystalline molecular orientation and *Univ.* 1968, 46, 97 22 Ishizuka, O. *Kogyo Kagaku Zasshi* 1962, 65,247 shape factor in equation (4) are used:  $\Delta n_a = 0.004$  and  $k_f = 23$  Magil, J. H. *Polymer* 1962, 3, 35  $4\pi/3$  for three-dimensional growth;  $\Delta n_a = 0.0065$  and  $k_f = 24$  Iwanami, T., Takai, R. and Kaneko, R. *Kobunshi Kagaku n* ( $l = 150$  Å) for two-dimensional growth;  $\Delta n_a = 0.013$  and 1972, 29, 139  $\pi l_c$  ( $l_c$  = 150 Å) for two-dimensional growth;  $\Delta n_a$  = 0.013 and 1972, 29, 139<br> $k_s$  = 1/2 $\pi d^2$  ( $d_s$  = 1000 Å) for one-dimensional growth. In 25 Marker, L., Hay, P. M., Tilley, G. P., Early, R. M. and  $k_f = 1/2\pi d_c^2$  ( $d_c = 1000$  Å) for one-dimensional growth. In these molecular orientations, the calculated curves become 26 Padden, F. J. and Keith, H. D. J. *AppL Phys.* 1959, 30, 1479 of the same order as those of experimental data. In particu-<br>lar, crystallization with two-dimensional growth provides<br>*J. Polym. Sci.* (A) 1965, 3, 3041 lar, crystallization with two-dimensional growth provides J. Polym. Sci. (A) 1965, 3, 3041<br>the best fit to the experimental data. Then, in the case of 28 Takayanagi, M. and Kusumoto, N. *Kogyo Kagaku Zasshi* the best fit to the experimental data. Then, in the case of <sup>28</sup> Takayanagi, M<br>non-isothermal crustallization of a non-isotronic melt with 1959, 62, 587 non-isothermal crystallization of a non-isotropic melt with 1959, 62, 587 Horio, M., Imamura, R., Ishizuka, O. and Fujiwara, H. *13th* highly oriented crystallizable molecules, the calculated value *Ann. Meeting Jpn Chem. Soc. Tokyo 1960* p 400 provides a better fit to the experimental data than the other 30 Danusso. F. and Gianotti, G. *Eur. Polym.* J. 1968, 4, 165

successively only highly oriented molecules can become B incorporated into crystallites. In the initial stage of crystallization, however, overall birefringence is very small. That is, only a small part of the supercooled melt can be nucleated Further, only molecules in the supercooled melt which have crystallites throughout the crystallization process in melt spinning. Hence, it is found that the crystallization process orientation of the supercooled melt in the very initial stage.

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